GLIFWC Wetlands Attachment

Analysis of Indirect Wetland Impacts from Groundwater Drawdown

Enclosed please find an analysis of indirect impacts to wetlands due to drawdown at the NorthMet mine site developed by the Great Lakes Indian Fish and Wildlife Commission (GLIFWC). GLIFWC is an intertribal agency exercising delegated authority from 11 federally recognized Ojibwe (or Chippewa) tribes in Wisconsin, Michigan and Minnesota. Those tribes have reserved hunting, fishing and gathering rights in territories ceded in various treaties with the United States. GLIFWC's mission is to assist its member tribes in the conservation and management of natural resources and to protect habitats and ecosystems that support those resources.

As you know, the proposed Polymet mine is located within the territory ceded in the Treaty of 1854. GLIFWC member tribes have expressed concern about the potential impacts of sulfide mining, whether those impacts occur within the 1854 ceded territory, in the 1842 ceded territory, which includes portions of Lake Superior, or the 1837 ceded territory. The following analysis is submitted by GLIFWC staff with the explicit understanding that each GLIFWC member tribe or any other tribe may choose to submit analysis and information from its own perspective.

Potential impacts to wetlands due to groundwater drawdown at the NorthMet mine site are described in the NorthMet Project Wetland Data Package Version 7 dated March 1, 2013 and summarized in the 2013 PSDEIS. Potential impacts due to drawdown are assessed using an analog method where information from another site is used to provide a best guess as to how wetlands surrounding NorthMet might be affected. The data package states that this method came out of the Wetlands IAP process however it does not state that GLIFWC and other cooperating and reviewing agencies have objected to using this method. The objections are detailed in the comments that GLIFWC provided within the IAP process (Attachment A).

GLIFWC continues to believe that the analog method can be informative in the process. We also reiterate that the lead agencies' reliance on analogs as the only source of information to gauge impacts from pit dewatering is not a rigorous approach to impact estimation. However, because of the lead agencies insistence that this method be used in the SDEIS, GLIFWC is providing an independent analysis using information from other mine pits located on the Mesabi Range.

GLIFWC member tribes are: in Wisconsin -- the Bad River Band of the Lake Superior Tribe of Chippewa Indians, Lac du Flambeau Band of Lake Superior Chippewa Indians, Lac Courte Oreilles Band of Lake Superior Chippewa Indians, St. Croix Chippewa Indians of Wisconsin, Sokaogon Chippewa Community of the Mole Lake Band, and Red Cliff Band of Lake Superior Chippewa Indians; in Minnesota -- Fond du Lac Chippewa Tribe, and Mille Lacs Band of Chippewa Indians; and in Michigan -- Bay Mills Indian Community, Keweenaw Bay Indian Community, and Lac Vieux Desert Band of Lake Superior Chippewa Indians.

Analog Data Used

- Randal Property Wells T3 and T4 (Source: Crotteau, 2013), Rhino and Highway 7 wells in the vicinity of the Canisteo pit. (Source: Adams and Liljegren 2011)
- MNDNR observation well, in the vicinity of Hibtac pits (Source: Crotteau, 2013).
- Dom-ex and Pinto wells north of Hibbing in the vicinity of Hibtac (Source: Crotteau, 2013).
- Keewatin City wells #1 and #2 in the vicinity of the Keetac pit (Source: Liesh and Associates Technical Memorandum, 2009).

Contour lines showing the analog well information in relation to the proposed NorthMet mine site are provided in Figure 1.

Wetland Analog Impact Zones and Significance Criteria

GLIFWC objections to the impact zones developed by the lead agencies are presented in Attachment A. We believe these distance zones are somewhat arbitrary and continue to have concerns regarding their use. Despite these concerns, we are using similar impact zones so that the results we present can be compared to the analysis that in presented in the NorthMet Project Wetland Data Package Version 7.

GLIFWC impact zones (Figure 2) are:

- Zone 1 0 to 1000 feet from the mine pit edge.
- Zone 2 1000 to 2000 feet from the mine pit edge.
- Zone 3 2000 to 5000 feet from the mine pit edge.
- Zone 4 5000 to 10000 feet from the mine pit edge.

For impact assessment, this analysis applies the significance criteria outlined in large table 8 of the NorthMet Project Wetland Data Package Version 7. However, GLIFWC does not automatically exclude wetlands that have been classified as ombotrophic in the data package from being considered impacted by drawdown. Literature indicates that ombotrophic wetlands can and are impacted by drawdown. Several studies document vegetation changes at ombotrophic bogs in Finland (Murphy et al, 2009, Grootjans et al 2009, Jaatinen et al 2006, Vassander 1995). In general, groundwater drawdown beneath these ombotrophic bogs leads to increases in the root mass of woody vegetation species as well as greater dominance of woody species at the surface. The functions and values changes resulting from the drawdown induced change in vegetation in ombotrophic bogs are not characterized in the PSDEIS.

The analysis in the NorthMet Project Wetland Data Package Version 7 relies on surface observations of plant communities to classify bog wetlands as ombotrophic or minerotrophic. GLIFWC agrees that this is useful information but we maintain that it is not a substitute for detailed understanding of the relationship of the water table and wetlands at the site. NorthMet Project Wetland Data Package Version 7 states that hydraulic conductivity in the unconsolidated deposits around the mine site can range between 0.012 to 31 feet per day. This range of values indicates that substantial water movement within the aquifer can occur. Therefore unless there is information on whether the unconsolidated deposits that underlie wetlands are saturated or not it

is not possible to know the degree to which groundwater supports wetland hydrology. Despite the assumption in the wetlands section of perched conditions for over 50% of wetlands at the mine site, Section 4.2.2-5 of the PSDEIS states that saturated conditions exist within the unconsolidated deposits and the underlying bedrock. It also states that recharge to the bedrock comes from leakage from the overlying surficial aquifer. Given these statements describing vertical movement of water in the mine site area, it does seem reasonable to also assume a vertical hydrologic connection between ombotrophic wetlands and the surficial aquifer.

The data package and PSDEIS assume that wetlands deemed to be ombotrophic are not connected to groundwater and therefore are not impacted by drawdown. This assumption is based mostly on plant lists and surface observations. We believe that this assumption is not supportable. Instead, GLIFWC assumes that there is at least a partial connection between ombotrophic wetlands and groundwater. Therefore, if groundwater under these "perched" wetlands is drawn down by several feet, this new head pressure would lead to impacts to the wetlands because of a "bathtub effect". In other words, water would seep out of ombotrophic wetlands in areas where there is a hydrologic connection to the saturated layer. This assumption is the support for assigning significance criteria for Deep Mersh/Shallow Marsh and Open bog wetlands for the Crandon project. It is this project that is the basis for the significance criteria used in the PSDEIS (large table 8 of the NorthMet Project Wetland Data Package Version 7).

Finally, the data package ignores the fact that the proposed NorthMet pits would be over twice the depth of a typical pit located up on the Mesabi Range and double the depth of the Canisteo pit analog. Thus the hydrologic effects on the surrounding aquifer will likely be greater for the NorthMet project.

Zone 1 Impacts (0 - 1000 Feet)

Wetlands within Zone 1 are depicted in Figure 3. Information provided by MNDNR Mining Hydrologist Michael Crotteau indicates that 2 wells at the Randall property (Wells T3 and T4) were artesian before a drain tile was installed to reduce groundwater levels in the area. This indicates a strong hydrologic connection between these wells and the Canisteo pit approximately 700 feet from the edge of the pit (Figure 4). The basement of the Randall residence was built when the Canisteo pit was dewatered is at an elevation of 1300 feet above sea level. The surface elevation at the site is 1310.73 feet above sea level. This indicates at least an 8 to 10 foot increase in the elevation of the water table 792 feet away from a reflooded Canisteo pit.

Based on these analog wells, a drawdown of up to 10 feet could affect wetlands in zone 1. We believe it is reasonable to assume that 5 to 10 feet of drawdown would occur throughout zone 1. In addition, these wetlands are often remnants of wetlands directly impacted by the pits and stockpiles, are surrounded by roads and ditches, and directly border the pits. Therefore, all wetlands in zone 1 are assessed as severely impacted (Table 1).

UNIQUE ID	EGGERS & REED CLASS	ACRES	IMPACT	IMPACT DESCRIPTION
24	Alder thicket	5.920	Severe	Conversion of wetland type
33A	Alder thicket	142.927	Severe	Conversion of wetland type
43	Alder thicket	7.456	Severe	Conversion of wetland type
44	Alder thicket	14.704	Severe	Conversion of wetland type
45	Alder thicket	159.903	Severe	Conversion of wetland type
51	Alder thicket	5.542	Severe	Conversion of wetland type
52	Alder thicket	18.113	Severe	Conversion of wetland type
53D	Alder thicket	39.376	Severe	Conversion of wetland type
100	Coniferous bog	981.692	Severe	Possible conversion of wetland type
101	Coniferous bog	60.631	Severe	Possible conversion of wetland type
103	Coniferous bog	174.579	Severe	Possible conversion of wetland type
107	Coniferous bog	126.238	Severe	Possible conversion of wetland type
[*] 25	Coniferous bog	20.965	Severe	Possible conversion of wetland type
32	Coniferous bog	73.745	Severe	Possible conversion of wetland type
48	Coniferous bog	190.986	Severe	Possible conversion of wetland type
62	Coniferous bog	1.782	Severe	Possible conversion of wetland type
76	Coniferous bog	22.181	Severe	Possible conversion of wetland type
77	Coniferous bog	118.315	Severe	Possible conversion of wetland type
79	Coniferous bog	25.709	Severe	Possible conversion of wetland type
82	Coniferous bog	44.293	Severe	Possible conversion of wetland type
888	Coniferous bog	12.481	Severe	Possible conversion of wetland type
90	Coniferous bog	499.822	Severe	Possible conversion of wetland type
96	Coniferous bog	52.276	Severe	Possible conversion of wetland type
97	Coniferous bog	32.904	Severe	Possible conversion of wetland type
99	Coniferous bog	14.536	Severe	Possible conversion of wetland type
107A	Coniferous swamp	3.090	Severe	Change in vegetation
33B	Coniferous swamp	47.690	Severe	Change in vegetation
68	Coniferous swamp	172.129	Severe	Change in vegetation
72	Coniferous swamp	14.910	Severe	Change in vegetation
13	Deep marsh	54.139	Severe	Conversion of wetland type
20	Sedge meadow	2.237	Severe	Conversion to upland
107B	Shallow marsh	27.922	Severe	Conversion of wetland type
9	Shallow marsh	19.424	Severe	Conversion of wetland type

Table 1. Zone 1 impact assessment.

Zone 2 Impacts (1000 – 2000 Feet)

Wetlands within zone 2 are depicted in Figure 5. The Dom-ex well is located on the north side of the city of Hibbing is 1320 feet from the nearest dewatered pit at Hibtac. According to Mr. Crotteau this well experienced a drop of 3.07 feet in response to pit dewatering. Because wells in zone 3 (discussed below) indicate drawdown values ranging between 1 and 3 feet, and wells in zone 1 indicate dewatering of up to 10 feet, this analysis assumes that drawdowns in zone 2 are on the order of 3 to 5 feet. In addition to drawdown, wetlands in zone 2 are remnants of wetlands directly impacted by the project are surrounded by roads, ditches and other mine features, or have sections in zone 1. These wetlands can also be impacted by aerial deposition of mine related contaminants. The impact assessment for wetlands in zone 2 is outlined in Table 2.

It is important to note that a section of the upper Partridge River is located within Zone 2. Drawdowns of 3 to 5 feet under a river could severely reduce baseflow leading to reductions in flow in the river channel. Reductions in flow could indirectly impact riparian wetlands downstream.

UNIQUE ID	EGGERS & REED CLASS	ACRES	IMPACT	IMPACT DESCRIPTION
100A	Alder thicket	8.275	Moderate to Severe	Change in vegetation to change in wetland type
53D	Alder thicket	802.660	Moderate to Severe	Change in vegetation to change in wetland type
43	Alder thicket	9.150	Moderate to Severe	Change in vegetation to change in wetland type
53	Alder thicket	15.967	Moderate to Severe	Change in vegetation to change in wetland type
100A	Alder thicket	8.210	Moderate to Severe	Change in vegetation to change in wetland type
22C	Alder thicket or Shrub-carr	30.447	Moderate to Severe	Change in vegetation to change in wetland type
315	Alder thicket or Shrub-carr	185.118	Moderate to Severe	Change in vegetation to change in wetland type
100	Coniferous bog	49.041	Severe	Possible conversion of wetland type
48	Coniferous bog	556.958	Severe	Possible conversion of wetland type
62	Coniferous bog	108.797	Severe	Possible conversion of wetland type
80	Coniferous bog	3.138	Severe	Possible conversion of wetland type
[*] 86	Coniferous bog	4.866	Severe	Possible conversion of wetland type
88	Coniferous bog	14.561	Severe	Possible conversion of wetland type
100	Coniferous bog	105.174	Severe	Possible conversion of wetland type
104	Coniferous bog	4.747	Severe	Possible conversion of wetland type
90	Coniferous bog	383.229	Severe	Possible conversion of wetland type
773	Coniferous bog	53.424	Severe	Possible conversion of wetland type
888	Coniferous bog	940.711	Severe	Possible conversion of wetland type
77	Coniferous bog	20.517	Severe	Possible conversion of wetland type
552	Coniferous bog	31.210	Severe	Possible conversion of wetland type
61	Coniferous swamp	3.727	Moderate to Severe	Possible changes in vegetation
701	Coniferous swamp	3.968	Moderate to Severe	Possible changes in vegetation
856	Coniferous swamp	74.335	Moderate to Severe	Possible changes in vegetation
22A	Coniferous swamp	9.564	Moderate to Severe	Possible changes in vegetation
53C	Coniferous swamp	28.741	Moderate to Severe	Possible changes in vegetation
48A	Coniferous swamp	7.821	Moderate to Severe	Possible changes in vegetation
57	Coniferous swamp	36.143	Moderate to Severe	Possible changes in vegetation
64	Hardwood swamp	3.290	Moderate to Severe	Change in vegetation to change in wetland type
47	Open bog	2.341	Severe	Change in vegetation to change in wetland type
90A	Open bog	78.350	Severe	Change in vegetation to change in wetland type
22B	Shallow marsh	29.190	Severe	Conversion of wetland type
16	Shallow marsh	3.317	Severe	Conversion of wetland type
22	Shallow marsh	15.372	Severe	Conversion of wetland type

Table 2. Zone 2 impact assessment.

Zone 3 Impacts (2000 – 5000 Feet)

GLIFWC has modified Zone 3 in response to available data (from 2000 to 3500 feet in data package to 2000 to 5000 feet). Wetlands within zone 3 are depicted in Figure 6. The Rhino and Highway 7 wells are 2150 and 2625 feet respectively from the Canisteo pit. In response to reflooding in the pit, the Rhino well responded with a greater than 1 foot increase and the Highway 7 well responded with a greater than 2 foot increase. Two additional wells provide analog information for this zone. First, the Pinto well north of Hibbing is 2112 feet from the nearest active pit shows a drop of at least 3.55 feet in response to pit dewatering. Second, a MNDNR observation well located 4224 feet from the nearest active pit at Hibtac shows a 3.5 foot drop in water level. Attachment B is a slide from a presentation given by Mr. Crotteau outlining the water level drop at this well.

In addition to these wells, the city of Keewatin has been greatly impacted by pit dewatering. Well #2 at approximately 4220 feet from the Mesabi Chief pit dropped 75 feet in response to a 150 foot drop in water levels in the pit. Water levels in Well #1 at approximately 4750 feet from the pit are also correlated with pit dewatering at the pit although the report indicates that the amount of water drop was less than at well #2. The correlations between pit

dewatering and water level drop at the wells were also supported by chemical characterization of the water in the pit (Attachment C).

These two wells are drilled into the bedrock and therefore it is not clear how those large water level drops in bedrock wells are expressed in the surficial aquifer and in wetlands. However, as previously stated, the PSDEIS does document vertical movement of water between the surficial aquifer and the bedrock aquifer. Regardless, this information fits with the analog approach of the lead agencies for NorthMet and illustrates that pit induced groundwater drawdowns can be expected to extend well into zone 3. The analog information suggests that drawdowns of 1 to 3.5 feet can be expected throughout zone 3. The impact assessment for zone 3 wetlands is provided in Table 3.

Zone 3 wetlands on the north side of the mine pits are also subject to impacts related to the dewatering of the Northshore pit. Figure 8 illustrates the possible extent of drawdown impacts at the Northshore pit based on the Hibtac well data provided by the MNDNR Mining Hydrologist Michael Crotteau. This cumulative effect is not included in version 7 of the data package or the PSDEIS. This analysis should be conducted.

It should also be noted that there are wetlands that fall within Zone 3 that have not been delineated by PolyMet. These wetlands should be delineated and the impacts of the combined Northshore and NorthMet drawdown on these wetlands should be assessed by the applicant.

Most of the east west reach of the Partridge River on the north side of the mine pits is within zone 3. As previously suggested, 1 to 3.5 feet of drawdown could be a significant impact to the hydrology of the river. In addition, the City of Kewaatin wells indicate that groundwater drawdown of tens of feet in the bedrock aquifer below the Partridge River are likely. This potential hydrologic impact should be assessed as part of the NEPA process. Finally, reductions in flow to the Partridge River could indirectly impact riparian wetlands downstream.

UNIQUE ID	EGGERS & REED CLASS	ACRES	IMPACT	IMPACT DESCRIPTION
53	Alder thicket	184.092	Moderate	Change in vegetation
53D	Alder thicket	714.287	Moderate	Change in vegetation
54B	Alder thicket	6.040	Moderate	Change in vegetation
54C	Alder thicket	8.015	Moderate	Change in vegetation
58	Alder thicket	372.266	Moderate	Change in vegetation
53D	Alder thicket	1283.309	Moderate	Change in vegetation
55	Alder thicket	15.732	Moderate	Change in vegetation
678	Alder thicket	1,676	Moderate	
				Change in vegetation
743	Alder thicket	4.750	Moderate	Change in vegetation
744	Alder thicket	10.344	Moderate	Change in vegetation
746	Alder thicket	3.572	Moderate	Change in vegetation
747	Alder thicket	10.027	Moderate	Change in vegetation
749	Alder thicket	99.326	Moderate	Change in vegetation
752	Alder thicket	36.908	Moderate	Change in vegetation
315	Alder thicket or Shrub-carr	2907.52	Moderate	Change in vegetation
565	Alder thicket or Shrub-carr	20.622	Moderate	Change in vegetation
566	Alder thicket or Shrub-carr	63.204	Moderate	Change in vegetation
480	Alder thicket or Shrub-carr	47.863	Moderate	
				Change in vegetation
555	Alder thicket or Shrub-carr	61.723	Moderate	Change in vegetation
557	Alder thicket or Shrub-carr	31.464	Moderate	Change in vegetation
890	Alder thicket or Shrub-carr	157.349	Moderate	Change in vegetation
106	Coniferous bog	581.72	Moderate to Severe	Change in vegetation
114	Coniferous bog	7.911	Moderate to Severe	Change in vegetation
406	Coniferous bog	26.125	Moderate to Severe	Change in vegetation
48	Coniferous bog	14.142	Moderate to Severe	Change in vegetation
552	Coniferous bog	31.738	Moderate to Severe	Change in vegetation
559		229.834	Moderate to Severe	
	Coniferous bog			Change in vegetation
562	Coniferous bog	56.744	Moderate to Severe	Change in vegetation
564	Coniferous bog	38.575	Moderate to Severe	Change in vegetation
62	Coniferous bog	20.018	Moderate to Severe	Change in vegetation
714	Coniferous bog	1692.646	Moderate to Severe	Change in vegetation
773	Coniferous bog	33.980	Moderate to Severe	Change in vegetation
774	Coniferous bog	88.486	Moderate to Severe	Change in vegetation
84	Coniferous bog	14.276	Moderate to Severe	Change in vegetation
84A	· · · · · · · · · · · · · · · · · · ·	55.627	Moderate to Severe	
	Coniferous bog			Change in vegetation
88	Coniferous bog	6.396	Moderate to Severe	Change in vegetation
887	Coniferous bog	1359.301	Moderate to Severe	Change in vegetation
888	Coniferous bog	1123.789	Moderate to Severe	Change in vegetation
90	Coniferous bog	685.002	Moderate to Severe	Change in vegetation
98	Coniferous bog	24.180	Moderate to Severe	Change in vegetation
984	Coniferous bog	162.094	Moderate to Severe	Change in vegetation
105	Coniferous bog	62.495	Moderate to Severe	Change in vegetation
11	Coniferous bog	95.587	Moderate to Severe	Change in vegetation
479	Coniferous bog	157.954	Moderate to Severe	Change in vegetation
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558	Coniferous bog	50.111	Moderate to Severe	Change in vegetation
697	Coniferous bog	48.894	Moderate to Severe	Change in vegetation
699	Coniferous bog	23.740	Moderate to Severe	Change in vegetation
713	Coniferous bog	80.451	Moderate to Severe	Change in vegetation
782	Coniferous bog	10.815	Moderate to Severe	Change in vegetation
783	Coniferous bog	20.604	Moderate to Severe	Change in vegetation
949	Coniferous bog	19.484	Moderate to Severe	Change in vegetation
53B	Coniferous swamp	4.626	Moderate	Minor vegetation change
53C	······································			Minor vegetation change
	Coniferous swamp	2.275	Moderate	
54	Coniferous swamp	44.113	Moderate	Minor vegetation change
54A	Coniferous swamp	34.455	Moderate	Minor vegetation change
54D	Coniferous swamp	17.547	Moderate	Minor vegetation change
553	Coniferous swamp	27.413	Moderate	Minor vegetation change
57	Coniferous swamp	293.943	Moderate	Minor vegetation change
701	Coniferous swamp	1642.996	Moderate	Minor vegetation change
745	Coniferous swamp	143.479	Moderate	Minor vegetation change
81	Coniferous swamp	13.507	Moderate	Minor vegetation change
856				· · · · · · · · · · · · · · · · · · ·
	Coniferous swamp	29.496	Moderate	Minor vegetation change
864	Coniferous swamp	1005.134	Moderate	Minor vegetation change
1145	Coniferous swamp	30.313	Moderate	Minor vegetation change
404	Coniferous swamp	137.651	Moderate	Minor vegetation change
53A	Coniferous swamp	25.257	Moderate	Minor vegetation change
53E	Coniferous swamp	20.088	Moderate	Minor vegetation change
554	Coniferous swamp	23.212	Moderate	Minor vegetation change
JJ-7	Oomerous swamp	20.414	Moderate	Minor vegetation change

Table 3. Zone 3 impact assessment.

Zone 4 Impacts (5000 – 10000)

Wetlands within zone 4 are depicted in Figure 7. There is no well data that can be used to draw conclusions about mine pit related drawdown in this zone. Based on Zone 3, it is reasonable to assume that 0 to 1 feet of drawdown would occur under wetlands within this zone.

As discussed above zone 4 wetlands on the north side of the proposed mine pits are also subject to impacts related to the dewatering of the Northshore pit (Figure 8).

UNIQUE ID	EGGERS & REED CLASS	ACRES	IMPACT	IMPACT DESCRIPTION
752	Alder thicket	36.908	None	None
53D	Alder thicket	1283.309	None	None
55	Alder thicket	15.732	None	None
58	Alder thicket	235.493	None	None
678	Alder thicket	1.676	None	None
743	Alder thicket	4.750	None	None
744	Alder thicket	10.344	None	None
746	Alder thicket	3.572	None	None
747	Alder thicket	10.027	None	None
749	Alder thicket	99.326	None	None
53	Alder thicket	130.786	None	None
480	Alder thicket or Shrub-carr	47.863	None to Moderate	None to vegetation change
555	Alder thicket or Shrub-carr	61.723	None to Moderate	None to vegetation change
557	Alder thicket or Shrub-carr	31.464	None to Moderate	None to vegetation change
566	Alder thicket or Shrub-carr	35.777	None to Moderate	None to vegetation change
890	Alder thicket or Shrub-carr	157.349	None to Moderate	None to vegetation change
315	Alder thicket or Shrub-carr	1256.836	None to Moderate	None to vegetation change
558	Coniferous bog	50.111	None	None
84A	Coniferous bog	41.351	None	None
11	Coniferous bog	95.587	None	None
105	Coniferous bog	62.495	None	None
90	Coniferous bog	230.686	None	None
479	Coniferous bog	157.954	None	None
559	Coniferous bog	228.822	None	None
564	Coniferous bog	33.827	None	None
697	Coniferous bog	48.894	None	None
699	Coniferous bog	23.740	None	None
713	Coniferous bog	80.451	None	None
714	Coniferous bog	1002.456	None	None
782	Coniferous bog	10.815	None	None
783	Coniferous bog	20.604	None	None
887	Coniferous bog	1128.525	None	None
888	Coniferous bog	90.125	None	None
949	Coniferous bog	19.484	None	None
106	Coniferous bog	451.616	None	None
54A	Coniferous swamp	16.573	None to Moderate	None to minor vegetation change
57	Coniferous swamp	20.917	None to Moderate	None to minor vegetation change
404				
	Coniferous swamp	137.651	None to Moderate	None to minor vegetation change
553	Coniferous swamp	18.531	None to Moderate	None to minor vegetation change
554	Coniferous swamp	23.212	None to Moderate	None to minor vegetation change
701	Coniferous swamp	852.230	None to Moderate	None to minor vegetation change
745	Coniferous swamp	82.463	None to Moderate	None to minor vegetation change
53A	Coniferous swamp	25.257	None to Moderate	None to minor vegetation change
891	Coniferous swamp	74.816	None to Moderate	None to minor vegetation change
864	Coniferous swamp	901.932	None to Moderate	None to minor vegetation change
1145	Coniferous swamp	30.313	None to Moderate	None to minor vegetation change
53E	Coniferous swamp	20.088	None to Moderate	None to minor vegetation change
899	Open bog	23.039	None	None
83	Open bog	16.555	None	None
83	Open bog	26.414	None	None
885	Open bog	950.076	None	None
889	Shallow marsh	3.279	None	None
17	Shallow marsh	12.072	None	None
1	Shallow marsh	4.560	None	None
3	Shallow marsh	3.808	None	None
6	Shallow marsh	6.654	None	None
29	Shallow marsh	126.876	None	None
	Shallow marsh	42.189	None	None
	OHABOW HAISH	42.100	NOTE	NOTE
708 709	Shallow marsh	18.496	None	None

Table 4. Zone 4 impact assessment.

Impacts to Riparian Wetlands along the Partridge River

The applicant and lead agencies have ignored repeated requests by cooperating agencies to better characterize the hydrology of the mine site through a robust surface and groundwater data collection program. Therefore reliable data with which to assess the effects of drawdown in the surficial and bedrock aquifers to riparian wetlands along the Partridge River are not available. Based on pit dewatering induced drawdowns at other sites described in this report, it is reasonable to assume that flow in the Partridge River would be significantly reduced if the NorthMet project proceeds as currently designed. This would have an effect on riparian wetlands far downstream. These effects are highly important because of the potential for increased methylation of mercury that is released by the project. To date, these potential impacts have not been characterized.

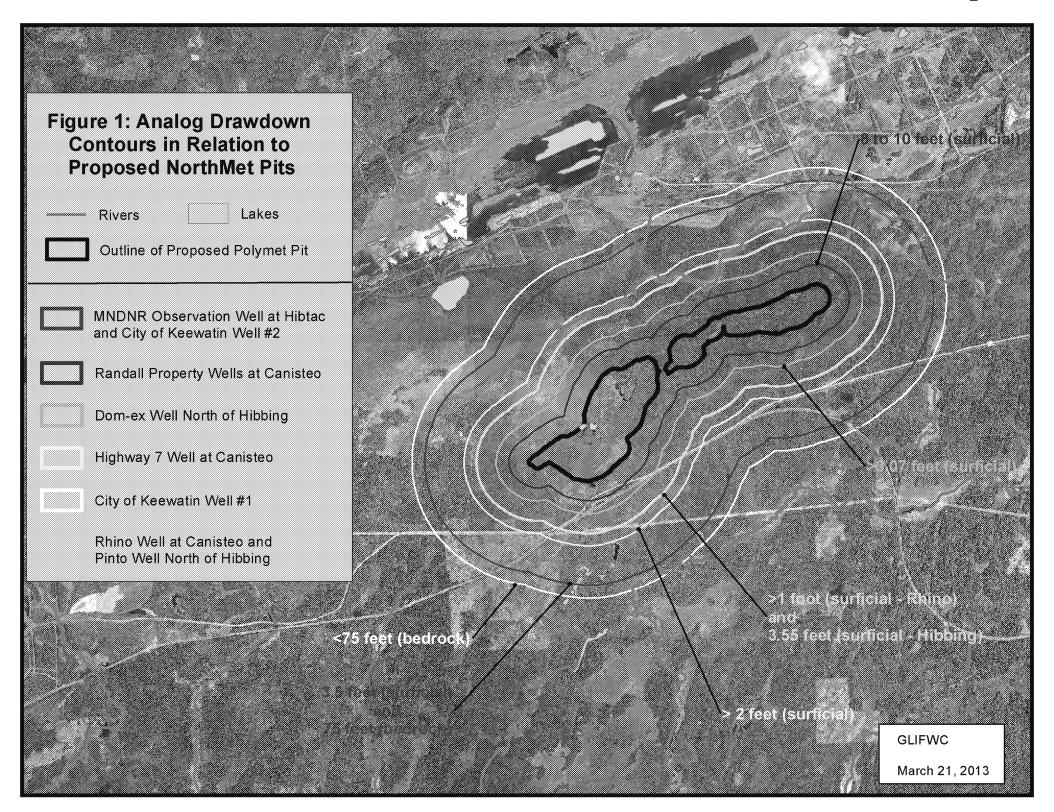
Summary

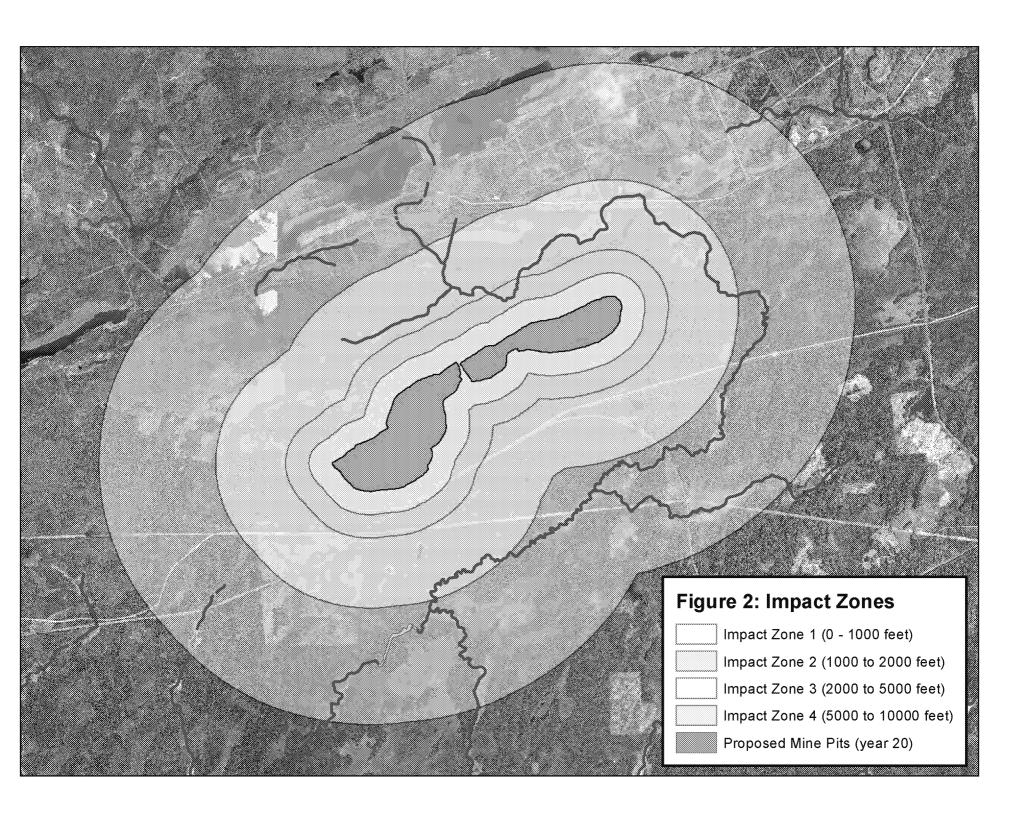
GLIFWC disagrees with the use of the Canisteo pit analog as the only method for estimating drawdown impacts for the NorthMet project. Repeated requests for a robust approach have not been successful. Therefore, this analysis uses the lead agencies own analog approach with data that is not included in the PSDEIS analysis. It is important to note that this analysis also uses the impact criteria developed for the Crandon project in Wisconsin which is the basis for impact criteria in the PSDEIS.

The assumption that ombotrophic bogs are completely separated from the surficial aquifer is not supportable. The extent of the hydrologic connection should be investigated.

Based on GLIFWCs analysis, wetlands severely impacted by drawdown total 3188.62 acres in zone 1; 2458.12 acres in zone 2; and 273.01 acres in zone 3. Severe indirect impacts to wetlands from mine pit drawdown total 5719.75 acres. All wetlands potentially impacted by drawdown are depicted in Figure 9. The Corps should require up front mitigation for all severely impacted wetlands. At a minimum, up front mitigation for all wetlands in zone 1 should be required. Additional up front mitigation should be considered for wetlands that are classified in the moderate to severe category. Robust monitoring is required for wetlands in the moderate category.

Impacts for wetlands suffering the cumulative effect of NorthMet and Northshore projects should be assessed and mitigation required. Un-delineated wetlands south of the Northshore pits should be delineated and included in the analysis. Impacts to riparian wetlands cannot be discounted given the shortcomings of the analog method and the inadequate characterization of surface and groundwater hydrology for the mine site area.





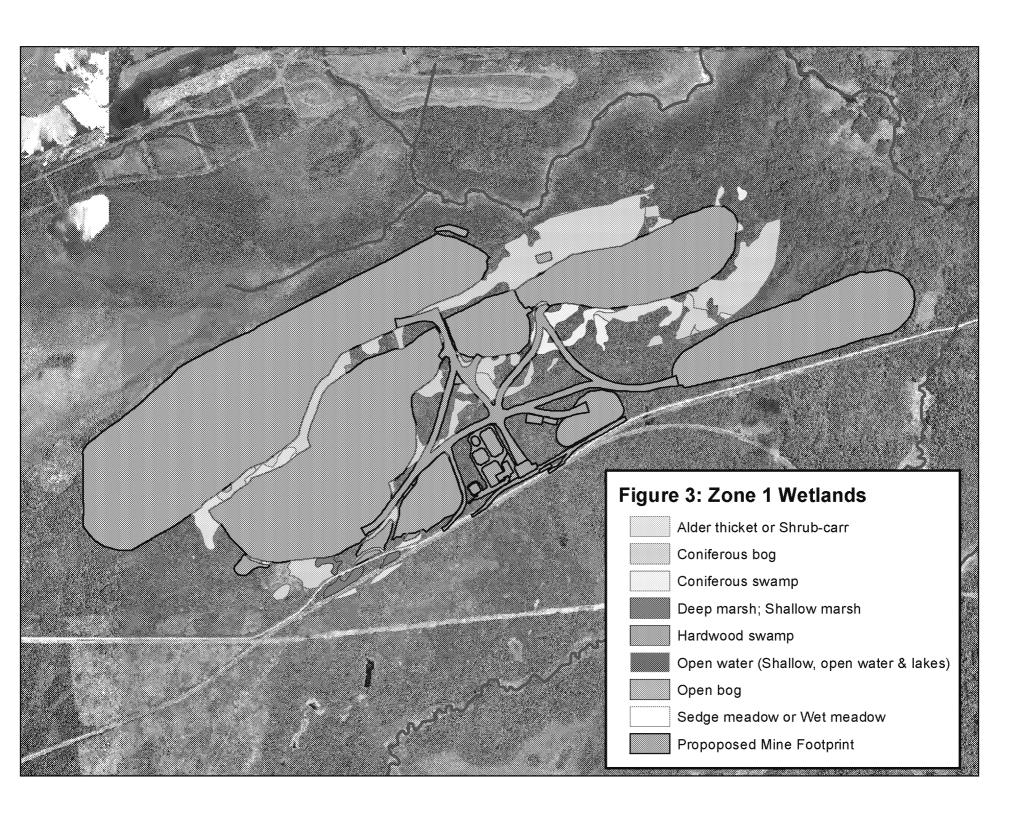
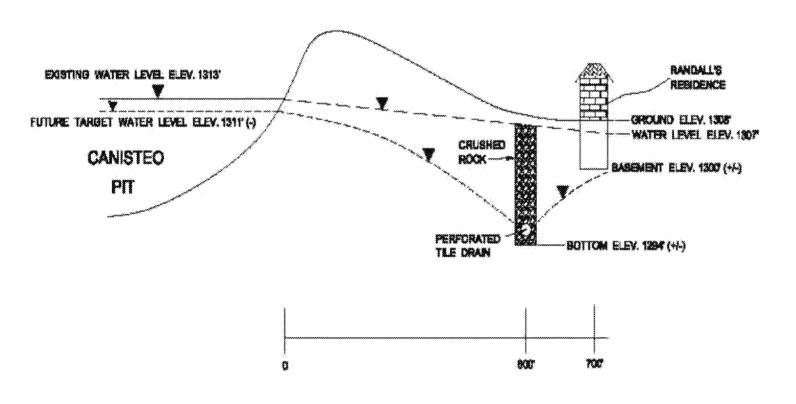




Figure 4

B

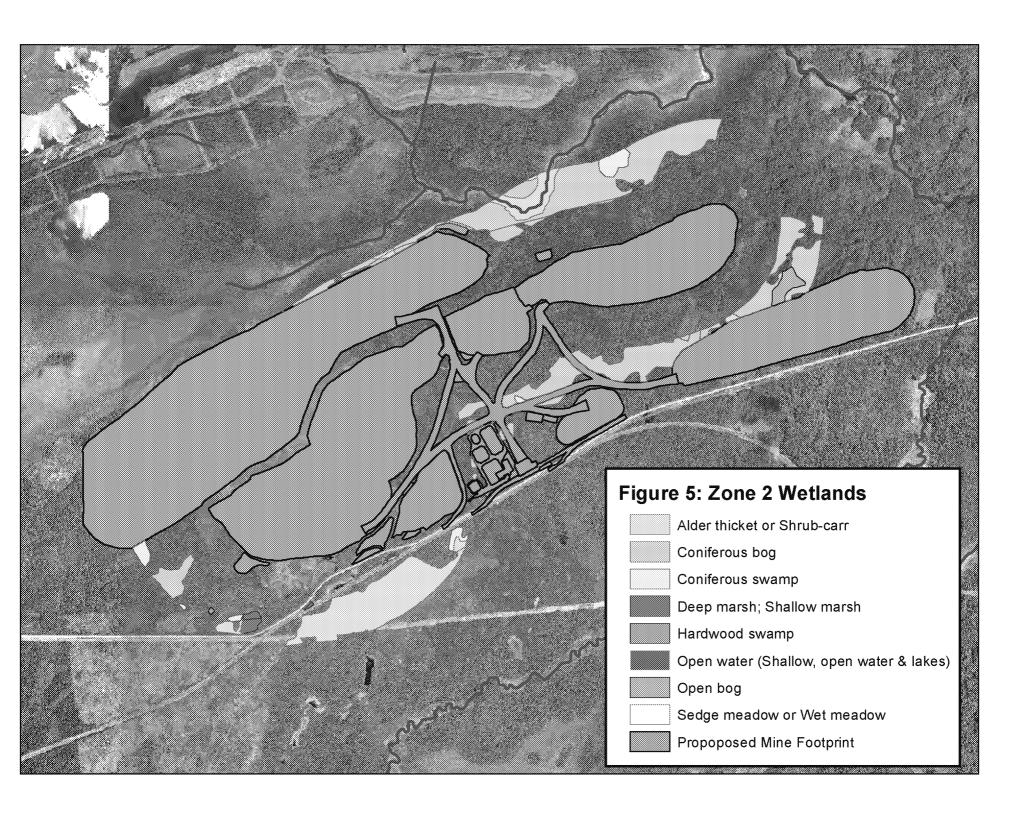


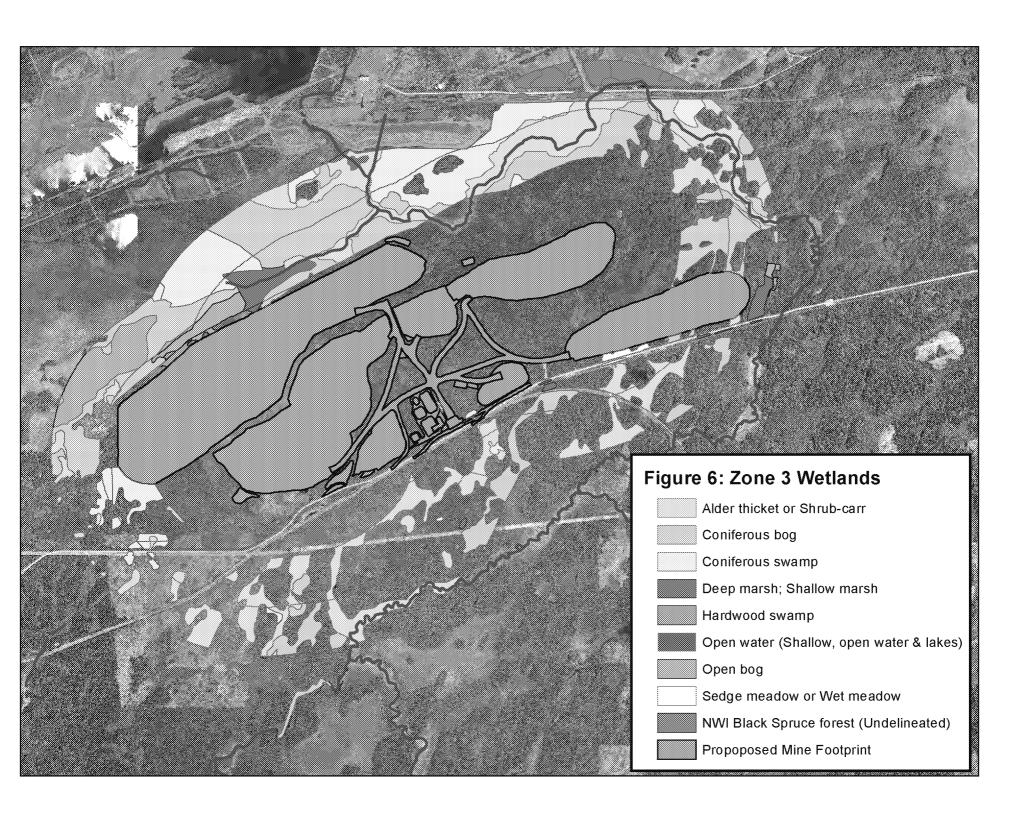


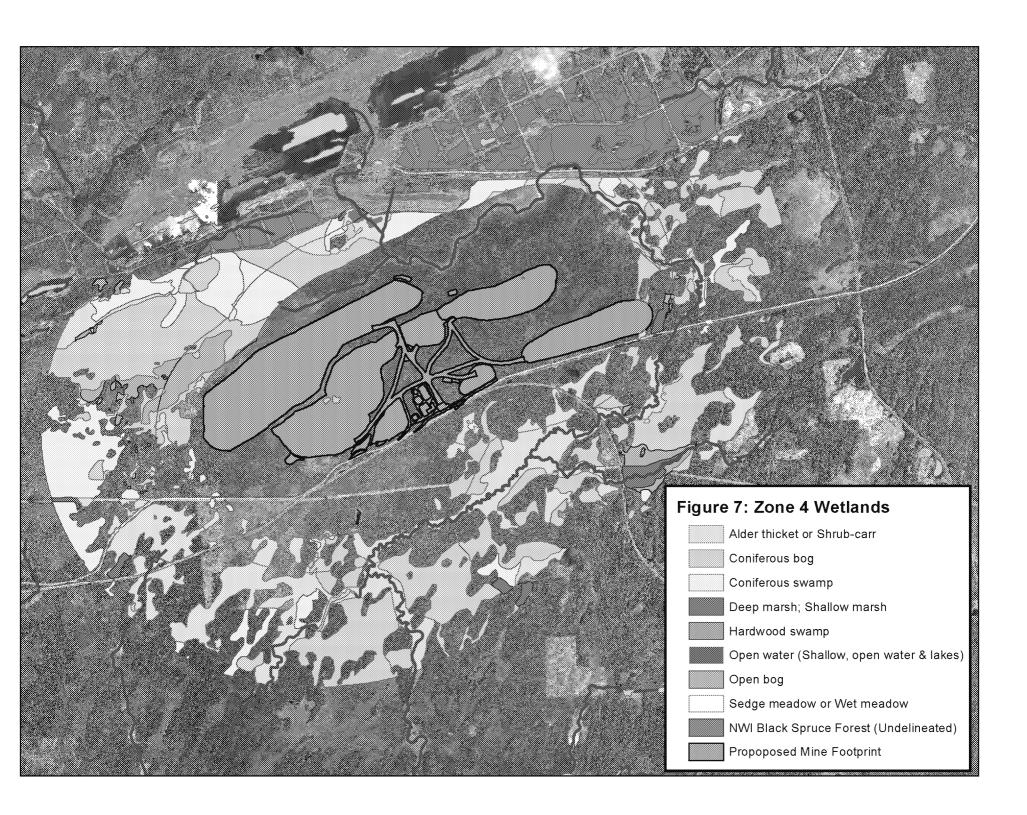
- EXIÓTINO WATER LEVEL

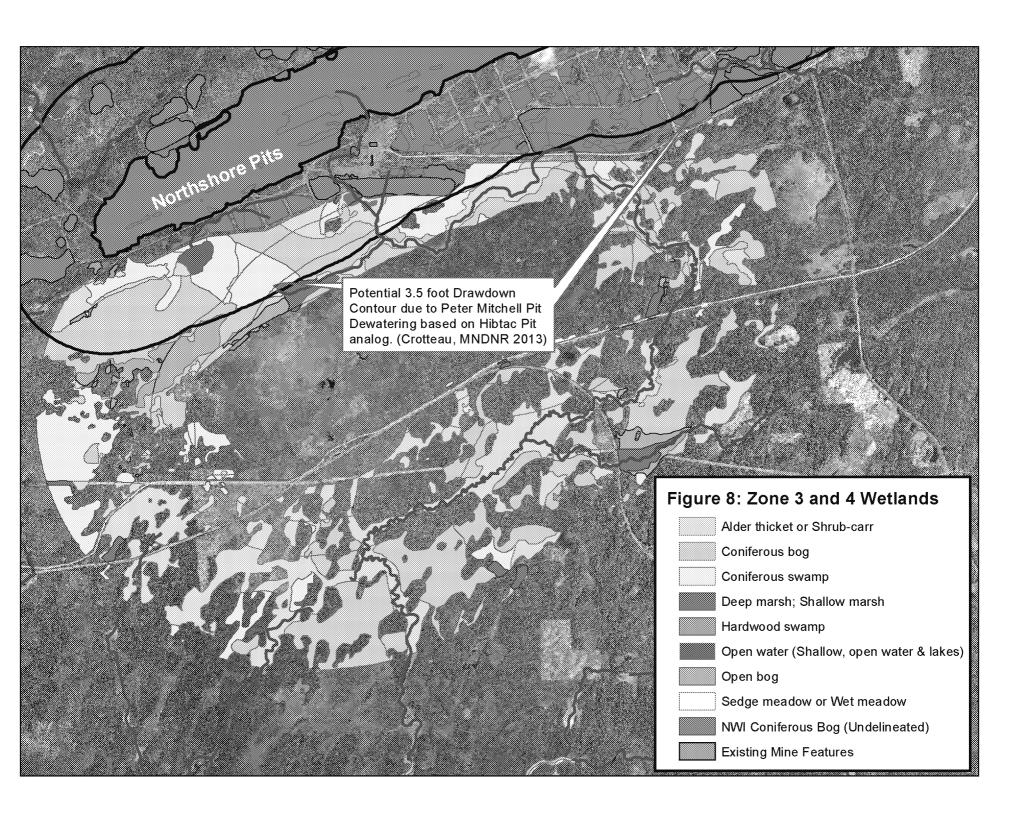
---- RITURE TARGET WATER LEVEL

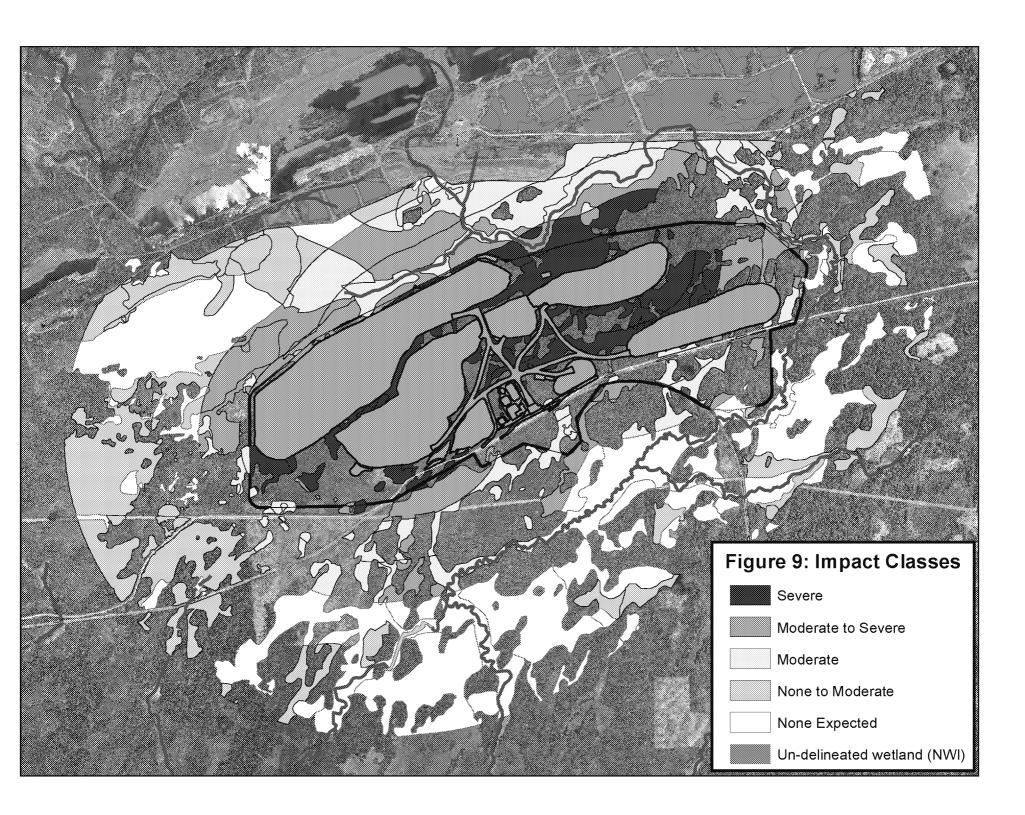
NOT TO SCALE











Attachment A

Wetland Resources IAP Draft Summary Memo

Line Number	Comments
General Comments (per line number)	[insert your name]
105	The Co-lead position described here is unchanged from the 2009 DEIS. This position is contrary to standard analysis that mining companies have to conduct as part of sulfide mine EIS processes across the country.
103	
118	This characterization requires further detail. According to our meeting notes, the need for a quantitative assessment of drawdown at the mine site was a unanimous position among the tribal cooperating agencies, the EPA, and the Fish and Wildlife Service. This position also received strong support from the PCA. This is why the original request by the wetland workgroup for a quantitative method of assessing drawdown impacts at the mine site was described as a "consensus". This should be clarified in the summary memo. See attached comment letter for additional detail on the groundwater modeling issue.
143	GLIFWC staff concur with Margaret Watkins that the cumulative impact assessment should be conducted for the same area that is used in the cultural resource assessment (Wetland area of potential effect). As discussed during the Wetland IAP call of May 13th 2011, baseline data for water quality in wetlands are essential to this analysis. We support the Corps
148	request that the applicant provide a list of available baseline data that will be assessed for adequacy in describing the existing condition and no action alternative. We request that this be specifically included in the workplan.
PolyMet NorthMet Project Co- Lead Agency Workplan Preparation Guidance for Wetland Assessment General Comments	
032	GLIFWC staff maintains that the analogue method proposed by the Army Corps does not provide sufficient information to base the indirect wetland impact analysis for the entire project. GLIFWC staff believe that the analysis area for cumulative impacts is not
078	adequate. See comment on line 143 of the summary memo. In addition, the cumulative impact assessment should cover topics that were not part of the 2009 DEIS. Climate change in the region is a stressor for wetlands. This additional factor should be assessed. Cumulative impacts of Iron Range mine projects on water quality of wetlands should be described.
085	GLIFWC staff do not agree with the Corps' definition of "reasonably foreseeable project". Several mine projects to the east and northeast of Polymet are likely to be proposed, some as early as this summer. A mining company interested in the Dunka deposit will be installing a stream gauge on the upper Partridge River this spring. Because this project will likely impact some of the same areas as Polymet (Partridge River watershed), this project should be included in the analysis.

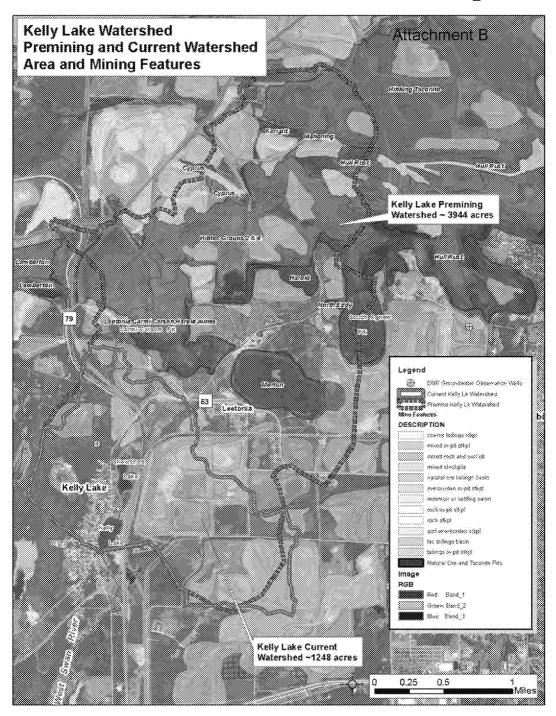
090	GLIFWC staff agree that the analogue data prepared by John Adams can be used as <u>part</u> of the indirect impact analysis. We remain concerned that this analysis is being used as the sole data source for the discussion of indirect wetland impacts at the Polymet mine site. As discussed during the wetland IAP call of May 13th 2011, a detailed report that includes all data and assumptions used by John Adams to assess the Canisteo Pit data should be developed and reviewed by the wetlands IAP group. After that review, a determination on the adequacy of the analysis as an analogue to Polymet can be made.
102	GLIFWC staff believe that these distances are open to a great deal of interpretation. We do not believe that the distance categories listed in this document are conservative interpretations of the Canisteo pit data.
118	The Canisteo Pit data indicated that water levels at a well 2300 feet from the pit were correlated with water fluctuations in the pit. Therefore it is inappropriate to

118

123

For the same reason stated in the comment on line 118, it is not appropriate to exclude the "high likelihood" or "moderate likelihood" of impact from this distance category.

exclude the "high likelihood" category from this distance category.



REVISED Attachment C REVISED



Liesch Associates, Inc. ■ 13400 15th Avenue North ■ Minneapolis, MN 55441 Phone: (763) 489-3100 ■ Toll Free: (800) 338-7914 ■ Fax: (763) 489-3101

TECHNICAL MEMORANDUM

TO: Mike Johnson, PE - Liesch Associates, Inc.

FROM: Jim de Lambert, PG - Liesch Associates, Inc.

DATE: February 18, 2009

RE: Water Supply Contingency Plans for Keewatin and Nashwauk

U.S. Steel – Minnesota Ore Operations (US Steel) is proposing to increase production at the US Steel Corporation Keewatin Taconite Facility under a project known the Keetac Expansion Project (the "Project"). The Project involves continuous dewatering operations that are ongoing and will continue in current and future mining areas. These planned activities are expected to generate drawdown in the aquifer locally and potentially at the water supply wells for the Cities of Keewatin and Nashwauk.

This memorandum is intended to provide background on the City water supplies and the Biwabik Iron Formation and to outline a plan to monitor the effects of mine pit dewatering on the aquifer so that appropriate steps can be taken to maintain the water supplies.

Relatively little information exists concerning the hydrogeology of the Biwabik Iron Formation (BIF) and the City water supplies. The Minnesota Department of Health (MDH) has assisted both Cities with Wellhead Protection activities and the results of this work probably represent the most comprehensive source of information concerning the source of water discharging at the City wells. In conducting this work it was apparent that traditional groundwater flow models would not be appropriate tools to estimate capture zones in the fractured BIF Aquifer. Instead, MDH utilized isotopic and chemical characteristics of water from the wells and nearby surface water bodies to estimate the source of water discharging at the wells. This work is summarized in separate reports titled Wellhead Protection Plan for the City of Keewatin - Part I (Walsh 2003) and Wellhead Protection Plan for the City of Nashwauk - Part I (Walsh 2007). Each report includes a delineation of the Wellhead Protection Area (WHPA), determination of the Drinking Water Supply Management Area (DWSMA) and assessments of Well and DWSMA Vulnerability. In addition, the reports include a summary of the hydrogeologic

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conditions concerning the city water supplies. Additional information used in preparing this memorandum includes various published maps and reports and personal communication with representatives from MDH, Department of Natural Resources and the Cities.

Keetac Mine Hydrogeology

The Keetac Mine extracts iron ore from the Biwabik Iron Formation (BIF) of the Mesabi Iron Range. The BIF is Precambrian in age, was deposited under marine conditions and is composed primarily of chert and iron minerals. Its subcrop area extends along strike for a distance of at least 100 miles generally from Grand Rapids to Babbitt and varies in width from one to three miles. The BIF has an overall thickness 350 to 750 feet and dips generally to the south at three to twelve degrees (Grout 1951). Information provided by the MDH from a deep test hole drilled near Keewatin suggests a BIF thickness of 590 feet in this area.

According to a suggestion by J. F. Wolf in 1917, and elaboration by J. W. Gruner in 1946 (Grout 1951), the BIF is generally divided into four members. From top to bottom, these are Upper Slaty, Upper Cherty, Lower Slaty, and Lower Cherty. The low grade magnetic iron ores, known as taconite, are mined from the Upper Cherty and Lower Cherty members. The Upper Cherty Member has a thickness ranging from 80 to 250 feet. The Lower Cherty ores are typically 120 to 425 feet thick. The slaty units can alter to form a sticky, clayey rock that generally exhibits low permeability including the Intermediate Slate which is a thin bedded silicate taconite, also known as paint rock that occurs at the base of the Lower Slaty Member. This is an important marker horizon for water supply purposes as it marks the contact with the Lower Cherty Member. Borehole logs suggest that the more productive zones for water supply wells may occur below this contact in the Lower Cherty Member.

In addition to being an important source of iron ore the BIF is also an important aquifer locally. Both Nashwauk and Keewatin, and numerous other range Cities and water users, utilize the BIF Aquifer. Depending on the amount of water desired and other factors, BIF aquifer wells are typically constructed by drilling a casing to solid rock, usually the top of the BIF Formation, and then drilling an open hole to a sufficient depth to obtain the required quantity of water. Yields in the 300 to 600 gallon per minute (gpm) range have been reported from existing wells. For Nashwauk and Keewatin, geochemical work conducted by MDH has indicated that a significant percentage of the water discharging at some of the wells originates from nearby mine pits.

The BIF Aquifer consists primarily of fine grained chert and iron minerals, exhibiting very little primary porosity. Groundwater movement appears to be restricted to zones of secondary permeability controlled by fractures and joints particularly in the cherty portions of the BIF. The MDH has conducted a suite of borehole logs at available wells constructed in the BIF Aquifer in an attempt indentify preferred flow paths and to further characterize the hydrogeology of the formation. This information suggests the occurrence of preferred flow zones in both of the cherty members.

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The Virginia Formation immediately overlies the BIF while the Pokegama Formation and the Giants Range Batholith underlay the BIF. These bedrock formations generally do not yield significant volumes of water to wells and are generally not considered important aquifers. Up to 200 feet of glacial drift lies above the consolidated bedrock near the Mesabi Range. Where these deposits include saturated granular outwash they may provide a potential source for significant volumes of water.

Little information is available regarding groundwater flow fields in the BIF due to a lack of available wells and detailed water level measurements over time. Mining operations conducted to date have undoubtedly altered natural flow patterns and planned mine dewatering activities in the Mesabi Range will continue to influence flow patterns.

Keewatin Water Supply

In recent years the City of Keewatin has obtained its water supply from two wells, designated Well 1 and Well 2. The City has indicated that it drilled an additional well in 2007, designated Well 3, in response to increasing manganese concentrations at Well 2. All wells are shown on the attached **Figure 1** (Attachment 1). Keewatin Well 3 has been added to the City's water supply system and Well 2 has been removed from service.

Basic information concerning Keewatin's wells is summarized on **Table 1** below and logs for each well are included in Attachment 2.

Table 1

Well	Well	Cas	sing	Open Hole, E	levation (ft msl)		
Name	Number	Diameter	Depth (ft)	Тор	Bottom	Status	Notes
1	192359	8-inch	249	1224	867	Active	Drilled in 1952/1982
2	228828	10-inch	344	1113	984	Observation	Drilled in 1951
3	751520	12-inch	198	1274	857	Active	Drilled in 2007

Water level information contained in Keewatin's Part 1 WHP plan shows a direct correlation between the dewatering of the Mesabi Chief Pit which was initiated in 1995 and Keewatin Well 2. As of 2002, the water level was lowered approximately 150 feet at the Mesabi Chief Mine while the static water level fell approximately 75 feet at Keewatin Well 2. Water levels were not collected at Keewatin Well 1 after 1998, however, the earlier measurements at Keewatin Well 1 also showed water level declines but somewhat less than those observed at Well 2. The WHP plan shows a correlation between water levels at select existing mine pits within the footprint of the proposed Project during dewatering and the water level at Well 2. The correlation was also supported by chemical characterization of water from the mine pits and well.

Details of the connection between mine dewatering, water levels and water chemistry at the City Wells are not clear. Long term monitoring is recommended to obtain additional Page 4 February 18, 2009 **REVISED**

information concerning the connection and to provide a mechanism to determine whether additional steps are needed to maintain the City's source of water supply.

Keewatin Water Use

The City of Keewatin is currently operating under Minnesota Department of Natural Resources (DNR) Appropriations Permit number 1972-2192. This permit allows Keewatin to pump up to 75 million gallons of water per year (mgy) at a permitted rate not to exceed 350 gallons per minute. The yearly reported pumping volumes submitted to the DNR are provided on **Table 2**. The reported values illustrate that the City's annual water use has increased from 45 to approximately 65 mgy in recent years.

Table 2

		Unique	Permit	Permit										
Permit	Well	Well No.	Vol (mgy)	Rate (gpm)	2007	2006	2005	2004	2003	2002	2001	2000	1999	1998
	1	192359			54.6	49.5	44.0	43.7	24.3	29.2	28.8	23.8	18.3	26.2
1979-2192	2	228828	75.0	350.0	8.8	14.5	16.2	16.9	29.2	15.8	17.1	22.8	25.8	18.2
	3	751520			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Ten Year A	verage	= 52.8 mgy	,	Total:	63.4	64.1	60.2	60.5	53.5	45.0	45.9	46.6	44.1	44.4

Nashwauk Water Supply

The water supply for the City of Nashwauk is obtained from two bedrock wells located within the City limits of Nashwauk as shown on **Figure 1**. Like Keewatin, both of Nashwauk's wells tap portions of the BIF Aquifer. Basic information concerning Nashwauk's wells is summarized on **Table 3** below and logs for each well are included in Attachment 2. Less information is available concerning Nashwauk's wells and some discrepancies exist regarding well numbering and depths. The well names and unique numbers used here are as presented in the MDH Wellhead Protection Plan Part 1, prepared for the City. The log for Well 3 indicates a casing depth of 40 feet in combination with a depth to bedrock of 110 feet. This is an unlikely scenario as the casing would typically extend at least to the top of the rock.

Table 3

Well	Well	Casing		Open Hole, E	levation (ft msl)		
Name	Number	Diameter	Depth (ft)	Тор	Bottom	Status	Notes
3	241017	8-inch	40	1449	1075	Active	Drilled in 1930
4	228819	16-inch	150	1289	899	Active	Drilled in 1947

The northern portion of the City of Nashwauk and the City's Well 3 are situated directly between two former natural ore pits, the Larue to the northeast and the Hawkins to the southwest. Well 4 is situated in the southern portion of the City approximately 3200 feet south of Well 3. Geochemical information provided in the MDH WHP report suggests that a significant percentage of water discharging at the wells originates at the Larue Pit. It is also likely that a connection exists between the levels in nearby mine pits and the

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City wells. To the northeast, the nearest mining proposed under the Keetac Project is more than two miles away. The effects of mine pit dewatering under this Project on the City wells will likely depend on the effects at the former natural ore pits between the Project and the City. Anecdotal evidence suggests that the former natural ore pits are separated by "land bridges" that may serve to reduce the effects of dewatering at the City wells.

To the southwest of Nashwauk, Minnesota Steel also has plans for taconite extraction, including mine pit dewatering and water supply pumping that could also affect water levels in nearby natural ore pits and the City wells.

Nashwauk Water Use

Nashwauk is currently operating under Minnesota Department of Natural Resources (DNR) Appropriations Permit number 1975-2151. This permit allows the City of Nashwauk to pump up to 70 million gallons of water per year (MGY) at a permitted rate not to exceed 1,100 gallons per minute. The yearly reported pumping volumes submitted to the DNR are provided on **Table 4**. Pumping in recent years has ranged from approximately 45 to 65 mgy.

Table 4

Permit				Permit Rate (gpm)		2006	2005	2004	2003	2002	2001	2000	1999	1998
1075 2151	4	228819	70.0										22.1	
1975-2151	3	241017	70.0	1,100.0	27.2	20.1	29.3	29.5	30.6	23.1	26.4	21.6	21.4	22.1
Ten Year A	\vera	ge = 52.5	mgy	Total:	52.3	46.0	57.1	63.6	63.9	55.9	52.0	45.2	43.4	45.8

Proposed Monitoring Plan

Monitoring is proposed to establish baseline conditions, to monitor changes in the BIF Aquifer that could impact the existing water supply wells for the Cities of Keewatin and Nashwauk and to assess potential measures to mitigate impacts, if necessary. Development and implementation of the Keetac Project will take place in stages over a period of several years. Sufficient time exists to monitor the resources in question and to develop a mitigation plan, if required. Impacts could include interference drawdown from dewatering activities or water supply pumping and/or changes in water quality that make use of the water undesirable. Therefore, the monitoring program should include both water quantity and quality components.

Water Quality

Existing water quality from both Cities supply wells should be obtained from the City and MDH. Additional baseline samples should be taken from existing wells for dissolved mineral constituents and general chemistry. Annual sampling of the wells should continue for select parameters to detect changes over time. Wells to be sampled include Nashwauk Wells 3 and 4 and Keewatin Wells 1 and 3. Parameter lists for

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baseline and annual sampling are included in Attachment 3.

The MDH has recommended that the Cities sample for stable isotopes of water, chloride and sulfate as part of their ongoing WHP efforts. MDH has indicated that they will conduct the analysis but the City would be responsible for obtaining the samples. US Steel representatives responsible for sample collection will contact MDH prior to sampling to coordinate collection of MDH samples with the sampling recommended here. The results could assist the Cities in their WHP efforts and provide useful information concerning the hydrogeology of the BIF Aquifer and the source of water discharging at the City wells.

Water Quantity

Long term water level monitoring points are required to assess drawdown in the aquifer. A search should be conducted to identify potential monitoring points including wells and surface water locations. MDH and DNR staff have expressed an interest in long term monitoring and noted a lack of available points in the BIF aquifer.

We understand that not all of the City wells involved are accessible for water level measurements. Arrangements should be made for the wells to be accessible and for City utility personnel to make regular measurements of static levels, pumping levels, pumping rates and volume.

Former Well 2 at Keewatin is now out of service and could serve as a useful monitoring point. We understand that the DNR has recently conducted logging procedures at the well and that both the DNR and MDH are interested in data from this location. The City has indicated that this well is available for long term monitoring by US Steel. A data logger and transducer will be installed and maintained by US Steel for well water level measurement at this location.

At present we are not aware of a suitable BIF Aquifer well for long term monitoring near Nashwauk. A new observation well is proposed for use as a dedicated monitoring point generally between the City and the Keetac project. This well should also be equipped with a transducer and data logger. Transducers and data loggers will be visited quarterly to verify operation, collect data and to reset the instruments to correct for drift.

Measurements of water levels from select mine pits, should also be collected as part of the Monitoring Plan. This includes water levels from pits within the Keetac Project, the LaRue pit complex and data collected by Minnesota steel for their operations southwest of Nashwauk. This information will be useful for correlating mine pit water levels with the City wells and the BIF Aquifer water levels in general.

Reporting

All data should be collected and summarized in a report format annually. The report should include a summary of the data collected during the previous year, a description of any changes to the monitoring network, recommended changes to the monitoring network and a determination as to any effects of the dewatering activities on the Cities well water supplies. If the results of the planned monitoring suggest significant changes in well water quality or level that may be related to Keetac mining activities, additional

Page 7 February 18, 2009 **REVISED**

monitoring activities may be recommended. The annual report will be prepared by US Steel no later than February 15th for the previous calendar year and distributed to the Cities, DNR and MDH for review.

Potential Mitigation Measures

In the event that mine dewatering activities have an adverse impact on the production or quality of the City water supply additional monitoring, treatment, augmentation or replacement of the impacted supply may become necessary. The hydrogeology of the Keewatin/Nashwauk area limits the available options to the following:

- Increased monitoring or changes to the monitoring plan if suspected impacts do not immediately threaten the City's ability to supply water.
- Modification of existing facilities including lowering, or replacing, existing pumps and deepening wells.
- New wells drilled in the BIF Aquifer in areas where interference effects are not as great.
- New wells drilled in the glacial outwash if areas of sufficient saturated thickness and favorable water quality can be identified.
- A new water treatment system to treat surface water, mine water or affected well water.

The extent of potential interference effects associated with the Project cannot be predicted with certainty at this time. The BIF Aquifer is utilized throughout the area and has the potential to supply adequate amounts of water to satisfy municipal needs. However, a better understanding of the effects of pumping on the BIF Aquifer is required to assess the potential for ongoing use and locations for additional BIF wells.

Glacial outwash deposits are utilized as municipal water sources throughout Minnesota. Although historical publications suggest that glacial outwash deposits are present between Keewatin and Nashwauk, glacial outwash deposits can change significantly over very short distances and specific investigations would be required to identify and assess the suitability for use as sources of water supply.

There are surface water resources in the area that could potentially provide a source of water including lakes that fill old mine pits and underground workings. It is anticipated that such a system would require construction of a surface water treatment plant.

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Select References

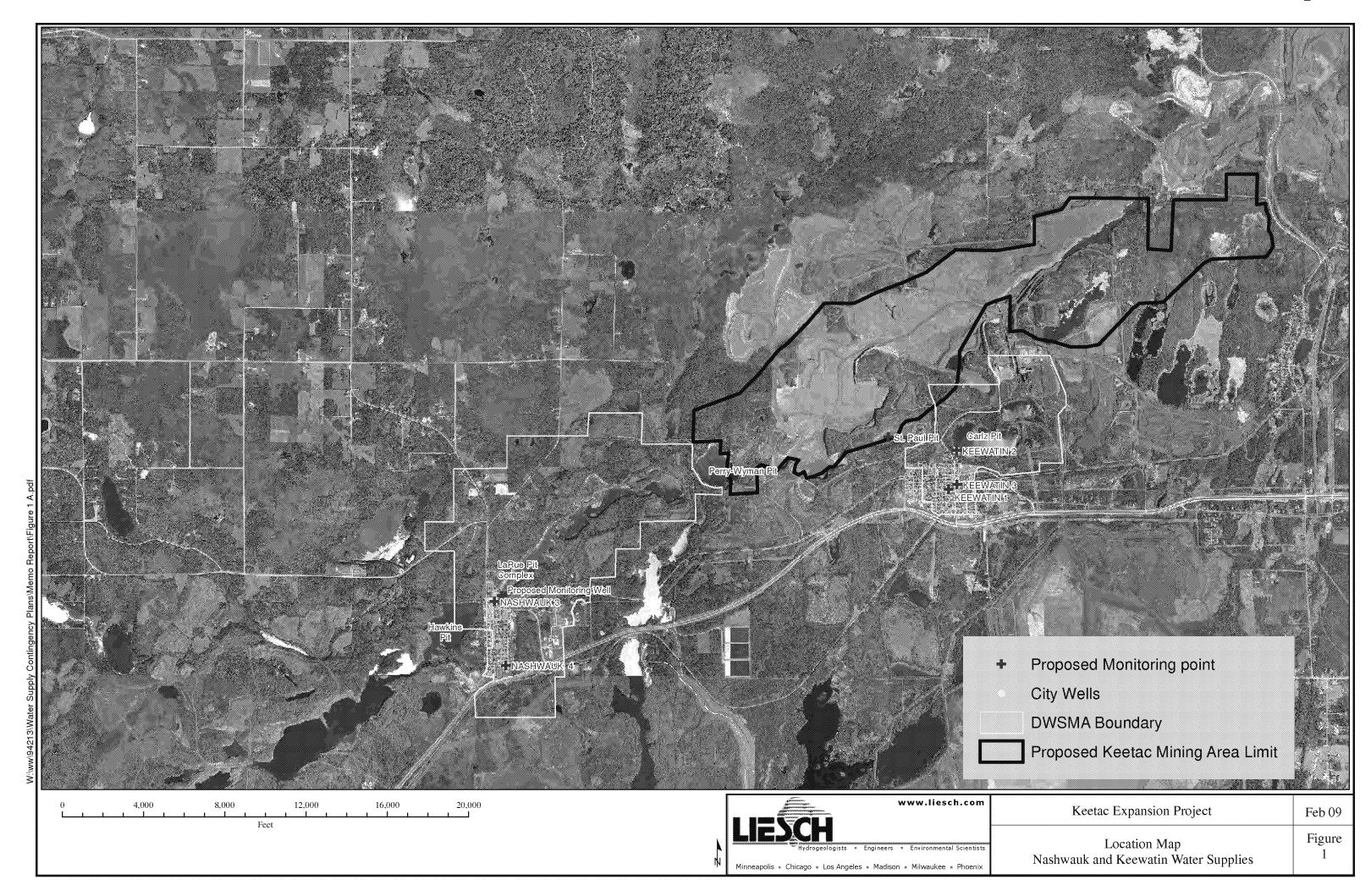
Grout, F. F., Gruner J. W., Schwartz G. M., and Thiel G. A. (1951) Precambrian Stratigraphy of Minnesota, Bulletin of the Geological Society of America, Volume 62, pages 1017-1078

Walsh, J. F. (2003) Wellhead Protection Plan for the City of Keewatin, Part 1 Delineation of the Wellhead Protection Area (WHPA), Drinking Water Supply Management Area (DWSMA) and Assessments of Well and DWSMA Vulnerability, Minnesota Department of Health, St. Paul, MN, 30 p.

Walsh, J. F. (2007) Wellhead Protection Plan, Part 1, Wellhead Protection Area Delineation, Drinking Water Supply Management Area Delineation, Well and Aquifer Vulnerability Assessments for the City of Nashwauk, Minnesota Department of Health, St. Paul, MN, 43 p.

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Attachment 1



Attachment 2

Unique No. 00192359 MINNESOTA DEPARTMENT OF HEALTH						Update Da	1/29		
County Name Itasca				D BORING RECORD		Entry Date	1992/08	3/03	
		***********		Statutes Chapter 1031					
Township Name Township 57	Range Dir Section 22 W 25	n Subse AB	ction DC	Well Depth Depth Co	ompleted ft.		Well Complet 2/11/03	ea	
Well Name KEEWATIN 1				Drilling Method Cable Tool					
Contact's Name KEE	EWATIN 1		***************************************	Drilling Fluid	⊥ Well ⊦	-lvdrofractu	red? Yes	: [] No	
				i watering i twee	From		ft. to	ft.	
KEEWATIN MN 55753				Use Community Supply (munic	cipal)				
					Yes	V N	Hole Diamet	er	
						[¥] , v	0 in. to	249 ft	
GEOLOGICAL MATERIAL	COLOR HARDNESS	FROM	то	Casing Diameter We	ight(lbs/	ft)	in. to	606 ft	
CLAY		Q	40	8 in. to 249 ft	Managar e e a caractería de la caractería d	28			
QUICKSAND		40	50						
CLAY		50	80						
QUICKSAND		80	90						
CLAY		90	180	Screen N	Open Ho	le From	249 ft. to	606 ft.	
SLATE		180	211	Make	7	Гуре			
DISSEMINATED TACONITE		211	216						
DISSEM, CHERTY & SLATY		216	281						
DISSEM. CHERTY & SLATY		281	471	Static Water Level 86 ft. from L	Land sur	face	Date	1982/10/13	
DISSEM. CHERTY TAC. & P		471	481	PUMPING LEVEL (below land s	urface)				
PAINT ROCK NON-MAG.		481	491	ft, after hrs	s. pumpi	ng	g.p.m.	*******************************	
DISSEM. CHERTY TAC. & P		491	496	Well Head Completion					
PORUS DISSEM. CHERTY T		496	526	Pitless adapter mfr Casing Protection			odel 12 in. above g	orade	
POURS DISSEM. CHERTY T		526	606	At-grade(Environmental Wells	s and Bo		19	,	
				Grouting Information We				No	
				Material From To (ft. G 0 185	.) Amo 239	nuill Aosins A			
				G 185 223	22	Y	*		
				G 223 249	0.3	Ň	9		
				Nearest Known Source of Conta					
				50 ft. direction	ammanc		type		
				Well disinfected upon completio	ın? ✓	Yes [No		
				Pump Not Installed		Date Ins	talled Y		
				Mfr name RED JACKET					
			*******************	Model	Н			460	
REMARKS, ELEVATION, SOU	RCE OF DATA, etc.		A	Drop Pipe Length 441 ft.		Cap	pacity 375	g.p.m	
ORIGIN CASING 12 INCH DIAI FEET.	METER TO 217			Type S					
WELL ORIGINALLY DRILLED BY MCCARTHY WELL CO. APRIL 1952.				Any not in use and not sealed wel Was a variance granted from the				No No	
USGS Quad: Keewatin	Elevation: 1473		MALLOONTDACTOR CERTIFICATION Lie O- C No. (040)						
Aquifer: PEBI Alt Id: 79-2192			Well CONTRACTOR CERTIFICATION Lic. Or Reg. No. 69183 License Business Name						
Rep	ort Copy				TERSO	<u>N, D.</u>			

Manual M	Unique No. 00228828	***************************************	·····			EPARTMENT OF HEALTH Update Date 2004/03/10
Township Name Township Range	County Name Itasca					
Mail Name KEEWATIN 2	Township Name Township	Range	Dir Sectio		*****	
Contact's Name		-				
Note	Well Name KEEWATIN 2					Drilling Method Cable Tool
Second Calles	Contact's Name KEI	EWATIN	2			Drilling Fluid Well Hydrofractured? Yes No
Canal	KEEWATIN MN 55753					From ft. to ft.
CLAY & BLUE			···		*****	Use Community Supply (municipal)
CLAY & BIG STONES BLUE 6 10 10 10 10 10 10 10						Casing Drive Shoe? Yes N Hole Diameter
CLAY & BIG STONES BLUE 6 10 24	GEOLOGICAL MATERIAL	COLOR	HARDNESS	FROM	то	Casing Diameter Weight(lbs/ft)
CLAY & BIG STONES, SAND RED 10	CLAY	BLUE		0	6	10 in. to 344 ft
CLAY & BIG BOULDERS BLUE 24 29 58 Screen N Open Hole From 344 ft. to 473 ft.	CLAY & BIG STONES	BLUE		6	10	***
Second Clay Second Composed Clay Second Clay S	CLAY & BIG STONES, SAND	RED		10	24	
Make Type Make Type Make Make Type Make Make Type Make Type Make Make Type Make Make Type Make Make Type Make	CLAY & BIG BOULDERS	BLUE		24	29	**
MUDDY SAND & BIG STONE	CLAY	BLUE	·	29	58	Screen N Open Hole From 344 ft. to 473 ft.
SANDY CLAY BLUE HARD 82 90	SANDY CLAY, SOME GRAV			58	73	Make Type
SLICE HARD 90 115 Static Water Level 279 ft. from Land surface Date 1951/00/00	MUDDY SAND & BIG STONE			73	82	
STATE	SANDY CLAY	BLUE	HARD	82	90	
DECOMPOSED TANCONITE 124 130 324 ft. after hrs. pumping 280 g.p.m.	CLAY	BLUE	HARD	90	115	Static Water Level 279 ft. from Land surface Date 1951/00/00
SOLID TACONITE	SLATE		***************************************	115	124	PUMPING LEVEL (below land surface)
DECOMPOSED TACONITE	DECOMPOSED TANCONITE		***************************************	124	130	324 ft. after hrs. pumping 280 g.p.m.
DECOMPOSED TACONITE	SOLID TACONITE	***************************************		130	133	•
PAINTY DECOMPOSED TAC	DECOMPOSED TACONITE	***************************************		133	143	
DECOMPOSED TACONITE				143	165	
DECOMPOSED TACONITE				165	170	Grouting Information Well grouted? Yes No
TACONITE	PAINTY DECOMPOSED TAC			170	201	
DECOMPOSED PAINTY CUT 208 212 SANDY DECOMPOSED TAC 212 220 Nearest Known Source of Contamination ft. direction type Well disinfected upon completion? Yes No Pump Not Installed Date Installed Y Mfr name Model HP 60 Volts PAINT ROCK 355 365 SAND & ORE (WATER) CHERTY TACONITE 369 374 REMARKS, ELEVATION, SOURCE OF DATA, etc. DOCUMPOSED TACONITE 208 212 220 Nearest Known Source of Contamination ft. direction type Well disinfected upon completion? Yes No Pump Not Installed Date Installed Y Mfr name Model HP 60 Volts Drop Pipe Length ft. Capacity 9.p.m Type	DECOMPOSED TACONITE		***************************************	201	205	
SANDY DECOMPOSED TAC 212 220 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 224 230 230 2345 235	TACONITE		V.HARD	205	208	
SOLID TACONITE LITTLE SL 220 224 230 230 2	DECOMPOSED PAINTY CUT	***************************************		208	212	~
DECOMPOSED TACONITE L 220 224 DECOMPOSED TACONITE L 230 345 DECOMPOSED TACONITE L 345 350 DEC. TACONITE & PAINT R 350 355 PAINT ROCK 355 365 SAND & ORE (WATER) 365 369 CHERTY TACONITE 369 374 REMARKS, ELEVATION, SOURCE OF DATA, etc. Well disinfected upon completion? Yes No No Mfr name Model HP 60 Volts Mfr name Model HP 60 Volts Drop Pipe Length ft. Capacity 9.p.m Type	SANDY DECOMPOSED TAC			212	220	
DECOMPOSED TACONITE L 224 230 230 345 Pump Not Installed Mfr name Model Date Installed Y DECOMPOSED TACONITE DECOMPOSED TACONITE ADDITIONAL DEC. TACONITE & PAINT R 345 350 355 Model HP 60 Volts DEC. TACONITE & PAINT R 350 355 PAINT ROCK 355 365 SAND & ORE (WATER) 365 369 CHERTY TACONITE 369 374 REMARKS, ELEVATION, SOURCE OF DATA, etc. Drop Pipe Length ft. Capacity 9.p.m Type	SOLID TACONITE LITTLE SL		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	220	224	
DECOMPOSED TACONITE 345 350 DEC. TACONITE & PAINT R 350 355 PAINT ROCK 355 365 SAND & ORE (WATER) 369 374 REMARKS, ELEVATION, SOURCE OF DATA, etc. Drop Pipe Length ft. Capacity 9.p.m Type	DECOMPOSED TACONITE L			224	230	Lucal total
DECOMPOSED TACONITE 345 350 Model HP 60 Volts DEC. TACONITE & PAINT R 350 355 PAINT ROCK 355 365 SAND & ORE (WATER) 365 369 CHERTY TACONITE 369 374 REMARKS, ELEVATION, SOURCE OF DATA, etc. Drop Pipe Length ft. Capacity 9.p.m Type	SLATY TACONITE			230	345	
DEC. TACONITE & PAINT R 350 355 PAINT ROCK 355 365 SAND & ORE (WATER) 365 369 CHERTY TACONITE 369 374 REMARKS, ELEVATION, SOURCE OF DATA, etc. Drop Pipe Length ft. Capacity 9.p.m Type	DECOMPOSED TACONITE			345	350	
SAND & ORE (WATER) 365 369 CHERTY TACONITE 369 374 REMARKS, ELEVATION, SOURCE OF DATA, etc. Drop Pipe Length ft. Capacity 4.p.m Type	DEC. TACONITE & PAINT R			350	355	·
CHERTY TACONITE 369 374 REMARKS, ELEVATION, SOURCE OF DATA, etc. Drop Pipe Length ft. Capacity 9.p.m WELL DEEPENED FROM 374 TO APPROX.473 AROUND 1960,	PAINT ROCK			355	365	
REMARKS, ELEVATION, SOURCE OF DATA, etc. Drop Pipe Length ft. Capacity g.p.m Type Type	SAND & ORE (WATER)			365	369	
WELL DEEPENED FROM 374 TO APPROX.473 AROUND 1960,	CHERTY TACONITE			369	374	
WELL DEEF ENED FROM 374 TO AFROX.473 AROUND 1960,	REMARKS, ELEVATION, SOU	IRCE OF	DATA, etc.	***************************************		
Any not in use and not sealed well(s) on property? Yes No	WELL DEEPENED FROM 374 CASING IS SLOTTED FROM 3		ROX.473 ARC	OUND 196	Ю,	

EPA-R5-2018-005870_0001321

USGS Quad:	Keewatin PEBI	Elevation:	1457 79-2192	Was a variance granted from			
	Report			License Business Name Name of Driller	MCCARTH	IY	

HE-01205-06 (Rev. 9/96)

Unique No. 00751520	:		DEPARTMENT OF HEALTH Update Date 2007/10/01	
County Name Itasca			D BORING RECORD a Statutes Chapter 1031 Entry Date 2007/08/23	
Township Name Township 57	Range Dir Section 22 W 25	n Subsection ABDADB	Well Depth Depth Completed Date Well Completed 615 ft. 615 ft. 2007/08/16	*************
Well Name KEEWATIN 3			Drilling Method Multiple methods used	
Contact's Name CIT P. O. BOX 190 KEEWATIN MN 55753	Y OF KEEWATIN		Drilling Fluid Well Hydrofractured? Yes ✔ Water From ft. to	No ft.
Well Owner's Name KEI 2ND E AV KEEWATIN MN 55753	EWATIN 3		Use Community Supply (municipal) Casing Drive Shoe? Yes N Hole Diameter in, to 86	0 ft
GEOLOGICAL MATERIAL	COLOR HARDNESS	FROM TO	Casing Diameter Weight(lbs/ft) in. to 19	8 ft
FILL	BROW SOFT	0 3	18 in. to 80 ft 70.59 in. to 619	5 ft
CLAY	BROW SOFT	3 7	12 in. to 198 ft 49.56	
SAND, GRAVEL, ROCKS	BROW SOFT	7 20		
SANDY CLAY	BROW SOFT	20 22	 .	
SAND & GRAVEL	BROW SOFT	22 32	Screen N Open Hole From 198 ft. to 615	5 ft.
GRAVEL & CLAY LAYERS	BROW SOFT	32 35	Make Type	coorrecter
CLAY & GRAVEL	GRAY SOFT	35 163		
SLATE & CLAY LAYERS	BLACK V.SOFT	163 164		
SLATE & CLAY LAYERS	BLACK V.SOFT	164 168	Static Water Level 186 ft. from Land surface Date 2007/	08/16
SLATE & CLAY LAYERS (SO	BLK/G V.SOFT	168 190	PUMPING LEVEL (below land surface)	
SLATE & QUARTZ	BLACK SFT-MED	190 195	370 ft. after 6 hrs. pumping 450 g.p.m.	
SLATE & QUARTZ	BLACK SFT-MED	195 245	Well Head Completion	
SLATE	GRN/G SFT-MED	245 265	Pitless adapter mfr Model Casing Protection 12 in. above grade	
SLATE & TACONITE (MAGN	GRN/B MED-HRD	265 315	Casing Protection ✓ 12 in. above grade ☐ At-grade(Environmental Wells and Borings ONLY)	
TACONITE (MAGNETIC) GR	VARIE HARD	315 450	Grouting Information Well grouted? ✓ Yes No	***************************************
TACONITE (MAGNETIC) RU	VARIE MED-HRD	450 470	Material From To (ft.) Amount(yds/bags) G 80 3 Y	
TACONITE (MAGNETIC)	VARIE HARD	470 585		
TACONITE (MAGNETIC)	GRN/G HARD	585 615		
			Nearest Known Source of Contamination 100 ft. direction E type SEW Well disinfected upon completion? Yes No	
			Pump ✓ Not installed Date Installed N Mfr name	***************************************
DEMADUS ELEVATION CO.	IDOE OF DATA	***************************************	Model HP Volts Drop Pipe Length ft. Capacity g.p.n	n
REMARKS, ELEVATION, SOL CALIPER, MULTI TOOL, & FLO	***************************************		Tuna	
MDH.	244 MILTERED 3-12-200	LUGGED FU	Any not in use and not sealed well(s) on property? ☐ Yes ✔ No	***************************************
GAMMA LOGGED 8-31-2007, I TRAEN.			Was a variance granted from the MDH for this Well? ☐ Yes ☑ No	
USGS Quad: Keewatin Aquifer: PEBI	Elevation: 14 Alt ld: 47		Well CONTRACTOR CERTIFICATION Lic. Or Reg. No. 1404 License Business Name	
Rep	ort Copy		Name of Driller <u>TONY/DAN</u>	

Unique No. 00241017			EPARTMENT OF HEALT	,	Update Date 2005/06/23
County Name Itasca			BORING RECO Statutes Chapter 1031	KU	Entry Date 1992/08/03
Township Name Township	Range Dir Section 22 W 32	Subsection BACD	Well Depth 414 ft.	Depth Completed	Date Well Completed 1930/00/00
Well Name NASHWAUK 3			Drilling Method		
			Drilling Fluid	Well I	lydrofractured?
			Use Community Su	pply (municipal)	
			Casing Drive	Shoe? Yes	N Hole Diameter
GEOLOGICAL MATERIAL	COLOR HARDNESS	FROM TO	Casing Diameter	Weight(lbs/	ft)
DRIFT		0 110	8 in. to 40	ft	w
BIWABIK OXIDES OF IRON		110 210			
BIWABIK, MASSIVE IRON F		210 414			
			Screen	Open Ho	le From ft. to ft.
			Make	7	- ype
			Static Water Level	ft. from	Date
			PUMPING LEVEL (bei		
			ft. after	hrs. pumpi	ng g.p.m.
			Well Head Completion	1	
			Pitless adapter mfr		Model
			Casing Protection At-grade(Environm	ental Wells and Bo	☐ 12 in. above grade rings ONLY)
			Grouting Information	Well groute	
			Nearest Known Source	on Contamination	
			ft.	direction	type
			Well disinfected upor	completion?	Yes No
			Pump Not Ins	stalled	Date Installed
			Model	Н	P Volts
REMARKS, ELEVATION, SOI	JRCE OF DATA, etc.		Drop Pipe Length	ft.	Capacity 450 g.p.m
DATE OF SAMPLE 11/73			Туре Т		
INFO FROM CITY CLERK			Any not in use and not		
USGS Quad: Nashwauk	Elevation: 148	9	Was a variance grante	d from the MDH for	this Well? Yes No
Aquifer: PEBI	an 5 7 51 61 51 11	2151	Well CONTRACTOR C		Lic. Or Reg. No.
Dar	art Cany		License Business Na Name of Driller	me	
veh	ort Copy	***************************************	Ivaine of Dfiller		

Unique No. 00228819	1		DEPARTMENT OF HEALT DISCRIMING RECO		Update Date 2005/06/23
County Name Itasca			Statutes Chapter 1031		Entry Date 1992/08/03
Township Name Township 57	Range Dir Section 22 W 32	Subsection CDAD	Well Depth 540 ft.	Depth Completed 540 ft.	Date Well Completed 1947/00/00
Well Name NASHWAUK 4			Drilling Method		
			Drilling Fluid	Well F	lydrofractured? Yes No
			Use Community Su	ipply (municipal)	
			Casing Drive	Shoe? Yes	N Hole Diameter
GEOLOGICAL MATERIAL	COLOR HARDNESS	FROM TO	Casing Diameter	Weight(lbs/	ft)
UPPER SLATEY ABSENT		0 144	16 in. to 150	ft	
UPPER CHERTY		144 335	•••		
LOWER SLATE		330 345			
LOWER CHERTY MEMBER	•••••••••••	345 540			
			Screen	Open Ho	ole From ft. to ft.
			Make	Т	Type
			Static Water Level 15	0 ft. from Land surf	face Date
			PUMPING LEVEL (bel	low land surface)	
			ft. after	hrs. pumpii	ng g.p.m.
			Well Head Completion Pitless adapter mfr	n	Model
			Casing Protection		12 in. above grade
			At-grade(Environm	iental Wells and Bo	rings ONLY)
			Grouting Information	Well groute	d?
			Nearest Known Source	ce of Contaminatio	n
			ft.	direction	type
			Well disinfected upor	1 completion?	Yes No
			Pump Not Ins	stalled	Date Installed
			Model	H	P Volts
REMARKS, ELEVATION, SOL	JRCE OF DATA, etc.		Drop Pipe Length	ft.	Capacity 450 g.p.m
LOCATED BY CITY CLERK			Type T		
			Any not in use and not		
USGS Quad: Pengilly	Elevation: 143	39	Was a variance grante	d from the MDH for	this Well? Yes No
Aquifer: PEBI		10024S02	Well CONTRACTOR (Lic. Or Reg. No.
Ren	ort Copy		License Business Na Name of Driller	me	

Attachment 3

Table 5 - Baseline and Annual Sampling Lists

Baseline List		Annual List	
Analyte	Units	Analyte	Units
Gross Alpha	pCI/L	Alkalinity. Total	ma/
Gross Beta	pC!/L	Arsenic	J/Sm
Uranium	ng/L	Barium	ma/L
Radium 226	pČI/L	Cadmium	mg/L
Radium 228	pCI/L	Caloium	mg/L
Radon 222	pCI/L	Carbonate/Bicarbonate	mg/L
Alkalinity, Total	mg/L	Chloride	mg/L
Arsenic	mg/L	Chromium	mg/L
Barium	mg/L	Fluoride	mg/L
Cadmium	mg/L	Hardness, Total	mg/L
Caloium	mg/L	Iron	mg/L
Carbonate/Bicarbonate	mg/L	pH, Lab	units
Chloride	mg/L	Lead	mg/L
Chromium	mg/L	Magnesium	mg/L
Fluoride	mg/L	Manganese	mg/L
Hardness, Total	mg/L	Mercury	mg/L
Iron	mg/L	Nitrogen, Nitrate +Nitrite	mg/L
pH, Lab	units	Potassium	mg/L
Lead	mg/L	Selenium	mg/L
Magnesium	mg/L	Silver	mg/L
Manganese	mg/L	Sodium	mg/L
Mercury	mg/L	Sulfate	mg/L
Nitrogen, Nitrate +Nitrite	mg/L	Thallium	mg/L
Potassium	mg/L	Dissolved Solids, Total	mg/L
Selenium	mg/L	Cation/Anion Ballance	***
Silver	mg/L		
Sodium	mg/L		
Sulfate	mg/L		
Thallium	mg/L		
Dissolved Solids, Total	mg/L		
Cation/Anion Ballance	*****		
Volatile Organic Compounds 465 F	l/gu		